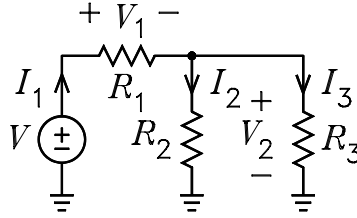


ECE3050 Homework Set 1

1. For $V = 18\text{ V}$, $R_1 = 39\text{ k}\Omega$, $R_2 = 43\text{ k}\Omega$, and $R_3 = 11\text{ k}\Omega$, use Ohm's Law, voltage division, and current division to solve for V_1 , V_2 , I_1 , I_2 , and I_3 .

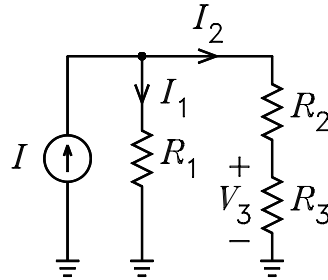


$$V_1 = 18 \frac{39\text{ k}\Omega}{39\text{ k}\Omega + 43\text{ k}\Omega \parallel 11\text{ k}\Omega} = 14.7\text{ V} \quad V_2 = 18 \frac{43\text{ k}\Omega \parallel 11\text{ k}\Omega}{39\text{ k}\Omega + 43\text{ k}\Omega \parallel 11\text{ k}\Omega} = 3.30\text{ V}$$

$$I_1 = \frac{18}{39\text{ k}\Omega + 43\text{ k}\Omega \parallel 11\text{ k}\Omega} = 376.8\text{ }\mu\text{A} \quad I_2 = \frac{11\text{ k}\Omega}{43\text{ k}\Omega + 11\text{ k}\Omega} I_1 = 76.8\text{ }\mu\text{A}$$

$$I_3 = \frac{43\text{ k}\Omega}{43\text{ k}\Omega + 11\text{ k}\Omega} I_1 = 300\text{ }\mu\text{A}$$

2. For $I = 250\text{ }\mu\text{A}$, $R_1 = 100\text{ k}\Omega$, $R_2 = 68\text{ k}\Omega$, and $R_3 = 82\text{ k}\Omega$, use Ohm's Law, voltage division, and current division to solve for I_1 , I_2 , and V_3 .

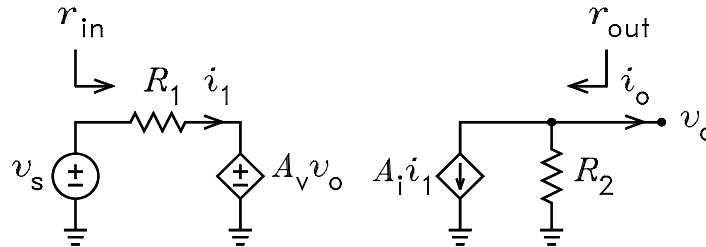


$$I_1 = 250\text{ }\mu\text{A} \frac{68\text{ k}\Omega + 82\text{ k}\Omega}{100\text{ k}\Omega + 68\text{ k}\Omega + 82\text{ k}\Omega} = 150\text{ }\mu\text{A}$$

$$I_2 = 250\text{ }\mu\text{A} \frac{100\text{ k}\Omega}{100\text{ k}\Omega + 68\text{ k}\Omega + 82\text{ k}\Omega} = 100\text{ }\mu\text{A}$$

$$V_3 = 100\text{ }\mu\text{A} \times 82\text{ k}\Omega = 8.2\text{ V}$$

3. It is given that $R_1 = 1\text{ k}\Omega$, $A_v = 10^{-4}$, $A_i = 50$, and $R_2 = 40\text{ k}\Omega$.



- (a) With $i_o = 0$, use superposition to write the equations for i_1 and $v_{o(oc)}$. Solve the equations for $v_{o(oc)}$ as a function of v_s .

$$i_1 = \frac{v_s - A_v v_o}{R_1} \quad v_{o(oc)} = -A_i i_1 R_2$$

$$v_{o(oc)} = \frac{-A_i \frac{R_2}{R_1}}{1 - A_i A_v \frac{R_2}{R_1}} v_s = -2500 v_s$$

(b) With $v_o = 0$, use superposition to write the equations for i_1 and $i_{o(sc)}$. Solve the equations for $i_{o(sc)}$ as a function of v_s .

$$i_{o(sc)} = -\frac{A_i v_s}{R_1} = -0.05 v_s$$

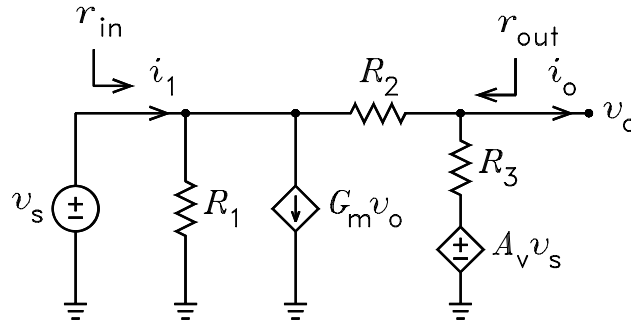
(c) Use the solutions for $v_{o(oc)}$ and $i_{o(sc)}$ to show that $r_{out} = 50 \text{ k}\Omega$.

(d) Show that the Thévenin equivalent circuit seen looking into the output is a voltage source $v_{o(oc)} = -2500 v_s$ in series with a resistance $r_{out} = 50 \text{ k}\Omega$.

(e) Show that the Norton equivalent circuit seen looking into the output is a current source $i_{o(sc)} = -0.05 v_s$ in parallel with a resistance $r_{out} = 50 \text{ k}\Omega$.

(f) If a load resistor $R_L = 20 \text{ k}\Omega$ is connected from the output node to ground, use both the Thévenin and the Norton equivalent circuits to show that $v_o = -714.3 v_s$ for both.

4. It is given that $R_1 = 10 \Omega$, $G_m = 0.5 \text{ S}$, $R_2 = 5 \Omega$, $R_3 = 50 \Omega$, and $A_v = 4$.



(a) With $i_o = 0$, use superposition to solve for $v_{o(oc)}$ as a function of v_s .

$$v_{o(oc)} = \frac{R_3}{R_2 + R_3} v_s + A_v v_s \frac{R_2}{R_2 + R_3} = \frac{R_3 + A_v R_2}{R_2 + R_3} v_s = 1.273 v_s$$

(b) With $v_o = 0$, use superposition to solve for $i_{o(sc)}$ as a function of v_s .

$$i_{o(sc)} = \frac{v_s}{R_2} + \frac{A_v v_s}{R_3} = v_s \left(\frac{1}{R_2} + \frac{A_v}{R_3} \right) = 0.28 v_s$$

(c) Solve for r_{out} .

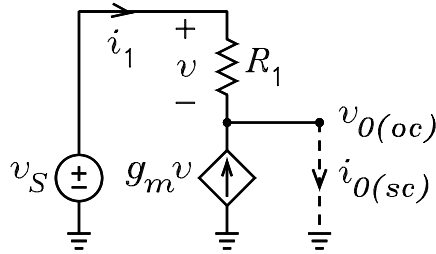
$$r_{out} = \frac{v_{o(oc)}}{i_{o(sc)}} = 4.545 \Omega$$

(d) Show that the Thévenin equivalent circuit seen looking into the output is a voltage source $v_{o(oc)} = 1.273 v_s$ in series with a resistance $r_{out} = 4.545 \Omega$.

(e) Show that the Norton equivalent circuit seen looking into the output is a current source $i_{o(sc)} = 0.28 v_s$ in parallel with a resistance $r_{out} = 4.545 \Omega$.

(f) If a load resistor $R_L = 5 \Omega$ is connected from the output node to ground, show $v_o = 0.667 v_s$.

5. It is given that $g_m = 0.025 \text{ S}$ and $R_1 = 40 \text{ k}\Omega$.



(a) With the output terminals open-circuited, use superposition of v_S and $g_m v$ to write equations for $v_{O(oc)}$ and v . Solve the two equations for $v_{O(oc)}$ as a function of v_S .

$$v_{O(oc)} = v_S + g_m v R_1 \quad v = 0 - g_m v R_1 \implies v = 0 \implies v_{O(oc)} = v_S$$

(b) For the output terminals short-circuited, use superposition of v_S and $g_m v$ to write equations for $i_{O(sc)}$ and v . Solve the two equations for $i_{O(sc)}$ as a function of v_S .

$$i_{O(sc)} = \frac{v_S}{R_1} + g_m v \quad v = v_S - 0 \implies v = v_S \implies i_{O(sc)} = v_S \left(\frac{1}{R_1} + g_m \right) = \frac{v_S}{39.96}$$

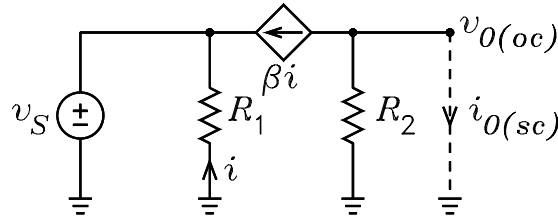
(c) Solve for the Thévenin equivalent circuit looking into the output terminals.

$$v_{O(oc)} = v_S \text{ in series with } r_{out} = 39.96 \Omega$$

(d) Solve for the Norton equivalent circuit looking into the output terminals.

$$i_{O(sc)} = \frac{v_S}{39.96} \text{ in parallel with } r_{out} = 39.96 \Omega$$

6. It is given that $\beta = 80$, $R_1 = 75 \text{ k}\Omega$, and $R_2 = 39 \text{ k}\Omega$.



(a) With the output terminals open-circuited, use superposition of v_S and βi to write equations for $v_{O(oc)}$ and i . Solve the two equations for $v_{O(oc)}$ as a function of v_S by eliminating i .

$$v_{O(oc)} = 0 - \beta i R_2 \quad i = \frac{-v_S}{R_1} \implies v_{O(oc)} = \frac{\beta R_2}{R_1} v_S = 41.6 v_S \text{ V}$$

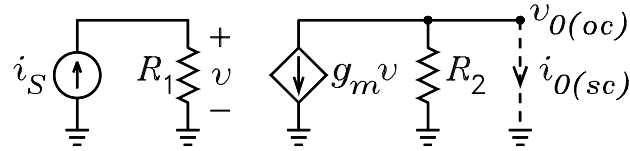
(b) With the output terminals short-circuited, use superposition of v_S and βi to write equations for $i_{O(sc)}$ and i . Solve the two equations for $i_{O(sc)}$ as a function of v_S by eliminating i .

$$i_{O(sc)} = 0 - \beta i \quad i = \frac{-v_S}{R_1} \implies i_{O(sc)} = \frac{\beta}{R_1} v_S = 1.067 v_S \text{ mA}$$

(c) Solve for the Thévenin equivalent circuit looking into the output terminals. [$v_{O(oc)} = 41.6 v_S$ in series with $39 \text{ k}\Omega$]

(d) Solve for the Norton equivalent circuit looking into the output terminals. [$i_{O(sc)} = 1.067 \times 10^{-3} v_S$ in parallel with $39 \text{ k}\Omega$]

7. It is given that $g_m = 0.002 \text{ S}$, $R_1 = 100 \text{ k}\Omega$, and $R_2 = 1 \text{ M}\Omega$.



- (a) With the output terminals open-circuited, solve for v as a function of i_S and $v_{O(oc)}$ as a function of v . Solve the two equations for $v_{O(oc)}$ as a function of i_S by eliminating v .

$$v_{O(oc)} = -g_m v R_2 \quad v = i_S R_1 \implies v_{O(oc)} = -g_m i_S R_2 R_1 = -2 \times 10^8 i_S$$

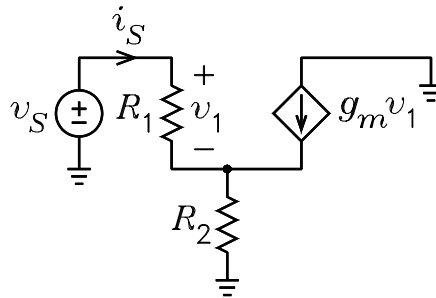
- (b) With the output terminals short-circuited, solve for v as a function of i_S and $i_{O(sc)}$ as a function of v . Solve the two equations for $i_{O(sc)}$ as a function of i_S by eliminating v .

$$i_{O(sc)} = -g_m v \quad v = i_S R_1 \implies i_{O(sc)} = -g_m i_S R_1 = -200 i_S$$

- (c) Show that the Thévenin equivalent circuit looking into the output terminals is a voltage source $v_{O(oc)} = -2 \times 10^8 i_S$ in series with a resistance $r_{out} = 1 \text{ M}\Omega$

- (d) Show that the Norton equivalent circuit looking into the output terminals is a current source $i_{O(sc)} = -200 i_S$ in parallel with a resistance $r_{out} = 1 \text{ M}\Omega$.

8. It is given that $R_1 = 3 \text{ k}\Omega$, $R_2 = 2 \text{ k}\Omega$, and $g_m = 0.1$. This problem illustrates two solutions for the input resistance to the circuit. In one solution, the source is a voltage source. In the other it is a current source.



- (a) Use superposition of v_S and $g_m v_1$ to solve for i_S .

$$i_S = \frac{v_S}{R_1 + R_2} - g_m v_1 \frac{R_2}{R_1 + R_2}$$

- (b) Use superposition of v_S and $g_m v_1$ to solve for v_1 .

$$v_1 = v_S \frac{R_1}{R_1 + R_2} - g_m v_1 R_1 \parallel R_2 \implies v_1 = v_S \frac{R_1}{R_1 + R_2} \times \frac{1}{1 + g_m R_1 \parallel R_2}$$

- (c) Solve the two equations for i_S as a function of v_S by eliminating v_1 .

$$\begin{aligned} i_S &= \frac{v_S}{R_1 + R_2} \left(1 - \frac{g_m R_2}{R_1 + R_2} \frac{R_1}{1 + g_m R_1 \parallel R_2} \right) = \frac{v_S}{R_1 + R_2} \left(1 - \frac{g_m R_1 \parallel R_2}{1 + g_m R_1 \parallel R_2} \right) \\ &= \frac{v_S}{R_1 + R_2} \frac{1}{1 + g_m R_1 \parallel R_2} = \frac{v_S}{605 \text{ k}\Omega} \end{aligned}$$

- (d) Solve for the input resistance to the circuit.

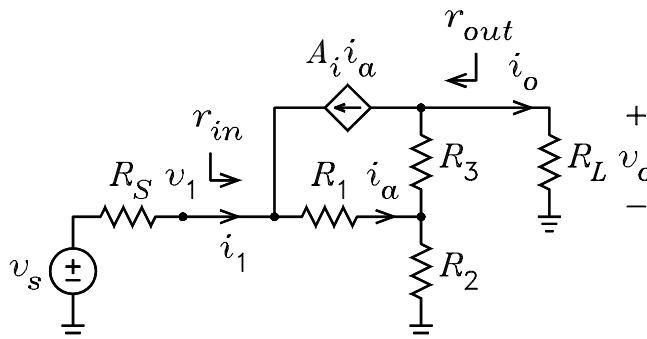
$$r_{in} = \frac{v_S}{i_S} = 605 \text{ k}\Omega$$

(e) Replace v_S with an independent current source i_S . Repeat the problem to solve for r_{in} . Which solution is simpler?

$$v_S = i_S (R_1 + R_2) + g_m v_1 R_2 \quad v_1 = i_S R_1 \implies v_S = i_S (R_1 + R_2 + g_m R_1 R_2)$$

$$r_{in} = \frac{v_S}{i_S} = R_1 + R_2 + g_m R_1 R_2 = 605 \text{ k}\Omega$$

9. The figure shows an amplifier equivalent circuit. It is given that $A_i = 0.99$, $R_S = 1 \text{ k}\Omega$, $R_1 = 25 \Omega$, $R_2 = 100 \Omega$, and $R_3 = 30 \text{ k}\Omega$.



- (a) With $R_L = \infty$, use superposition of v_s and $A_i i_\alpha$ to show that $v_{o(oc)}$ and i_α are given by

$$\begin{aligned} v_{o(oc)} &= v_s \frac{R_2}{R_S + R_1 + R_2} - A_i i_\alpha \left(R_3 + \frac{R_1}{R_S + R_1 + R_2} R_2 \right) \\ &= \frac{v_s}{11.25} - 29702.2 i_\alpha \end{aligned}$$

$$\begin{aligned} i_\alpha &= \frac{v_s}{R_S + R_1 + R_2} + A_i i_\alpha \frac{R_S + R_2}{R_S + R_1 + R_2} \\ &= \frac{v_s}{1125} + \frac{i_\alpha}{1.03306} \end{aligned}$$

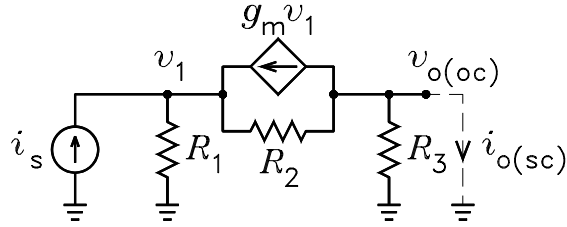
- (b) Solve the equations to show that $v_{o(oc)} = -824.97 v_s$.
(c) With $R_L = 0$, use superposition of v_s and $A_i i_\alpha$ to show that $i_{o(sc)}$ and i_α are given by

$$\begin{aligned} i_{o(sc)} &= \frac{v_s}{R_S + R_1 + R_2 \parallel R_3} \frac{R_2}{R_2 + R_3} - A_i i_\alpha \left(1 - \frac{R_S}{R_S + R_1 + R_2 \parallel R_3} \frac{R_2}{R_2 + R_3} \right) \\ &= \frac{v_s}{338525} - \frac{i_\alpha}{1.01309} \end{aligned}$$

$$\begin{aligned} i_\alpha &= \frac{v_s}{R_S + R_1 + R_2 \parallel R_3} + A_i i_\alpha \frac{R_S}{R_S + R_1 + R_2 \parallel R_3} \\ &= \frac{v_s}{1124.67} - \frac{i_\alpha}{1.13603} \end{aligned}$$

- (d) Solve the equations to show that $i_{o(sc)} = -v_s/136.486$.
(e) Solve for $r_{out} = v_{o(oc)}/i_{o(sc)}$. [$r_{out} = 112.597 \text{ k}\Omega$]
(f) With $R_L = 10 \text{ k}\Omega$, solve for v_o . [$v_o = -67.2913 v_s$]

10. For the circuit shown, it is given that $i_s = 4 \text{ mA}$, $R_1 = 2 \text{ k}\Omega$, $R_2 = 1 \text{ k}\Omega$, $R_3 = 9 \text{ k}\Omega$, and $g_m = 0.005 \text{ S}$.



- (a) Use superposition to solve for $v_{o(oc)}$. Express your answer in symbolic form.

$$\begin{aligned} v_1 &= i_s [R_1 \parallel (R_2 + R_3)] + g_m v_1 \frac{R_2}{R_1 + R_2 + R_3} R_1 \\ &= i_s \frac{R_1 \parallel (R_2 + R_3)}{1 - g_m R_1 \parallel (R_2 + R_3) + g_m \frac{R_2}{R_1 + R_2 + R_3} R_1} \\ v_{o(oc)} &= i_s \frac{R_1}{R_1 + R_2 + R_3} R_3 - g_m v_1 \frac{R_2}{R_1 + R_2 + R_3} R_3 \end{aligned}$$

- (b) Use superposition to solve for $i_{o(sc)}$. Express your answer in symbolic form.

$$\begin{aligned} v_1 &= (i_s + g_m v_1) R_1 \parallel R_2 = i_s \frac{R_1 \parallel R_2}{1 - g_m R_1 \parallel R_2} \\ i_{o(sc)} &= i_s \frac{R_1}{R_1 + R_2} - g_m v_1 \frac{R_2}{R_1 + R_2} \end{aligned}$$

- (c) Solve for the Thévenin equivalent circuit seen looking into the output terminal. Express your answer in numerical form.

$$v_{th} = v_{o(oc)} = -144 \text{ V} \quad R_{th} = \frac{v_{o(oc)}}{i_{o(sc)}} = -3150 \Omega$$

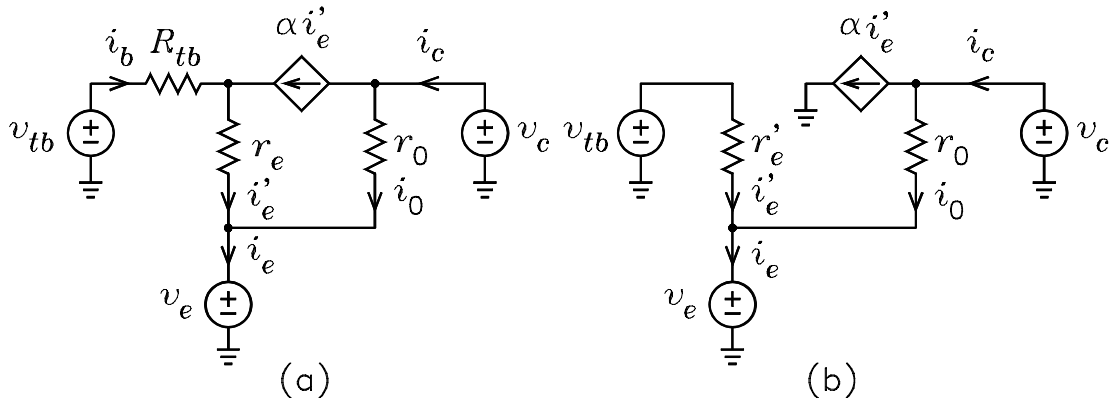
- (d) Solve for the Norton equivalent circuit seen looking into the output terminal. Express your answer in numerical form.

$$i_{nor} = i_{o(sc)} = 4.571 \text{ mA} \quad R_{nor} = \frac{v_{o(oc)}}{i_{o(sc)}} = -3150 \Omega$$

- (e) If a load resistor $R_L = 9 \text{ k}\Omega$ is connected to the output, what is the load voltage?

$$v_L = v_{th} \frac{R_L}{R_{th} + R_L} \text{ or } i_{nor} R_{nor} \parallel R_L = 57.6 \text{ V}$$

- 11.



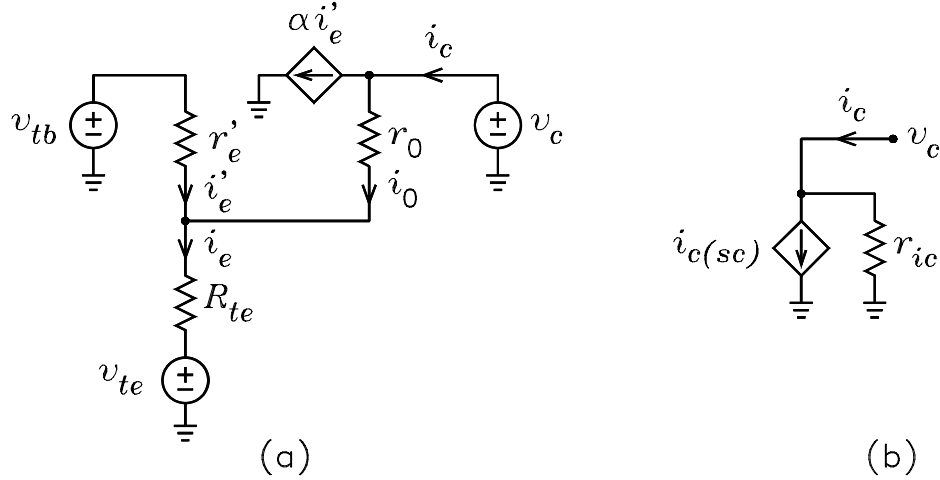
(a) For the circuit of figure (a), show that

$$i_b = (1 - \alpha) i'_e \quad i'_e = \frac{v_{tb} - v_e}{(1 - \alpha) R_{tb} + r_e} \quad i_0 = \frac{v_c - v_e}{r_0} \quad i_c = \alpha i'_e + i_0 \quad i_e = i'_e + i_0$$

(b) For the circuit of figure (b), show that i'_e , i_e , and i_c are the same as those in figure (a) provided r'_e is given by

$$r'_e = (1 - \alpha) R_{tb} + r_e$$

12.



(a) For the circuit of figure (a), use superposition of v_c , $\alpha i'_e$, v_{tb} , and v_{te} to show that

$$i_c = \frac{v_c}{r_0 + r'_e \parallel R_{te}} + \alpha i'_e - \frac{v_{tb}}{r'_e + R_{te} \parallel r_0} \frac{R_{te}}{R_{te} + r_0} - \frac{v_{te}}{R_{te} + r'_e \parallel r_0} \frac{r'_e}{r'_e + r_0}$$

$$i'_e = \frac{v_{tb}}{r'_e + R_{te} \parallel r_0} - \frac{v_{te}}{R_{te} + r'_e \parallel r_0} \frac{r_0}{r_0 + r'_e} - \frac{v_c}{r_0 + r'_e \parallel R_{te}} \frac{R_{te}}{R_{te} + r_0}$$

(b) Substitute the i'_e into the i_c equation to show that

$$i_c = \frac{v_{tb}}{r'_e + R_{te} \parallel r_0} \left(\alpha - \frac{R_{te}}{R_{te} + r_0} \right) - \frac{v_{te}}{R_{te} + r'_e \parallel r_0} \frac{\alpha r_0 + r'_e}{r_0 + r'_e}$$

$$+ \frac{v_c}{r_0 + r'_e \parallel R_{te}} \left(1 - \frac{\alpha R_{te}}{r'_e + R_{te}} \right)$$

(c) Show that the circuit of figure (b) gives the same value for i_c provided

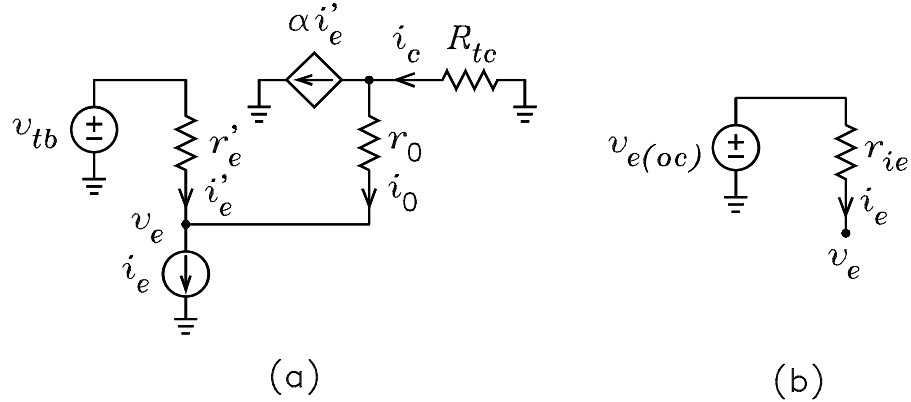
$$i_c = G_{mb} v_{tb} - G_{me} v_{te} + \frac{v_c}{r_{ic}} \quad G_{mb} = \frac{1}{r'_e + R_{te} \parallel r_0} \left(\alpha - \frac{R_{te}}{R_{te} + r_0} \right)$$

$$G_{me} = \frac{1}{R_{te} + r'_e \parallel r_0} \frac{\alpha r_0 + r'_e}{r_0 + r'_e} \quad r_{ic} = \frac{r_0 + r'_e \parallel R_{te}}{1 - \frac{\alpha R_{te}}{r'_e + R_{te}}}$$

(d) If β is sufficiently large, show that $G_{mb} = G_{me} = G_m$, where G_m is given by

$$G_m = \frac{1}{r'_e + R_{te}}$$

13.



(a) For the circuit of figure (a), use superposition of v_{tb} , i_e , and $\alpha i'_e$, to show that

$$v_e = v_{tb} \frac{r_0 + R_{tc}}{r'_e + r_0 + R_{tc}} - i_e [r'_e \parallel (r_0 + R_{tc})] - \alpha i'_e \frac{R_{tc} r'_e}{R_{tc} + r_0 + r'_e}$$

$$i'_e = \frac{v_{tb} - v_e}{r'_e}$$

(b) Eliminate i'_e between the equations to show that

$$v_e \left(1 - \frac{\alpha R_{tc}}{R_{tc} + r_0 + r'_e} \right) = v_{tb} \frac{r_0 + (1 - \alpha) R_{tc}}{r_0 + r'_e + R_{tc}} - i_e [r'_e \parallel (r_0 + R_{tc})]$$

(c) Show that the above equation simplifies to

$$v_e = v_{tb} \frac{r_0 + (1 - \alpha) R_{tc}}{r_0 + r'_e + (1 - \alpha) R_{tc}} - i_e \frac{r'_e (r_0 + R_{tc})}{r'_e + r_0 + (1 - \alpha) R_{tc}}$$

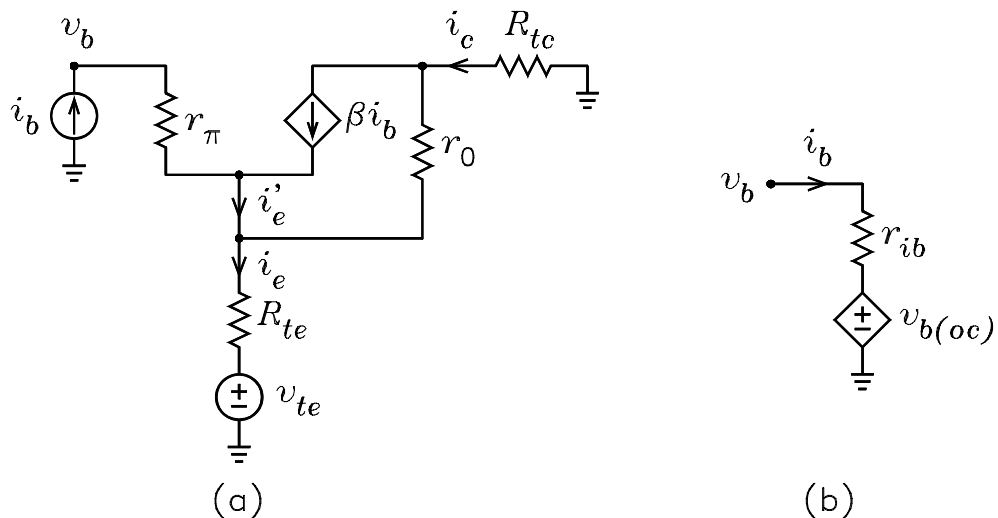
(d) Show that the circuit of figure (b) gives the same value for v_2 provided

$$v_{e(oc)} = v_{tb} \frac{r_0 + (1 - \alpha) R_{tc}}{r_0 + r'_e + (1 - \alpha) R_{tc}} \quad r_{ie} = \frac{r'_e (r_0 + R_{tc})}{r_0 + r'_e + (1 - \alpha) R_{tc}}$$

(e) If r_0 is sufficiently large, show that the above answers reduce to

$$v_{e(oc)} = v_{tb} \quad r_{ie} = r'_e$$

14.



(a) For the circuit of figure (a), use superposition of v_{te} , i_b , and βi_b to show that

$$v_b = v_{te} \frac{r_0 + R_{tc}}{R_{te} + r_0 + R_{tc}} + i_b [r_\pi + R_{te} \parallel (r_0 + R_{tc})] + \beta i_b \frac{r_0 R_{te}}{r_0 + R_{te} + R_{tc}}$$

(b) Show that the equation for v_b simplifies to

$$v_b = v_{te} \frac{r_0 + R_{tc}}{r_0 + R_{te} + R_{tc}} + i_b \left[r_\pi + R_{te} \frac{(1 + \beta) r_0 + R_{tc}}{r_0 + R_{te} + R_{tc}} \right]$$

(c) Show that the circuit of figure (b) gives the same value for v_b provided

$$v_{b(oc)} = v_{te} \frac{r_0 + R_{tc}}{r_0 + R_{te} + R_{tc}} \quad r_{ib} = r_\pi + R_{te} \frac{(1 + \beta) r_0 + R_{tc}}{r_0 + R_{te} + R_{tc}}$$

(d) If r_0 is sufficiently large, show that the above answers reduce to

$$v_{b(oc)} = v_{te} \quad r_{ib} = r_\pi + (1 + \beta) R_{te}$$