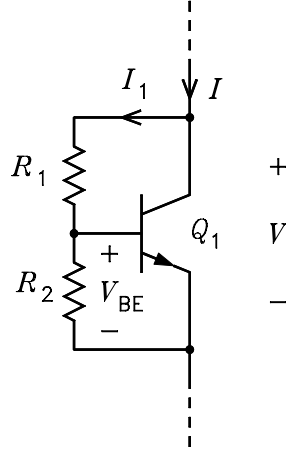


ECE3050 – Assignment 16

1. The figure shows a  $V_{BE}$  multiplier.



- (a) By writing a single node equation at the base node of  $Q_1$ , show that

$$I_1 = I_B + \frac{V_{BE}}{R_2} \implies V = V_{BE} \left( 1 + \alpha \frac{R_1}{R_2} \right) + \frac{I}{1 + \beta} R_1$$

Hint: Consider the emitter node to be the datum or zero voltage reference node and use

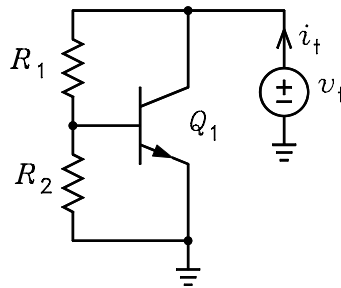
$$I_B = \frac{I_C}{\beta} = \frac{1}{\beta} (I - I_1) = \frac{1}{\beta} \left( I - \frac{V - V_{BE}}{R_1} \right)$$

- (b) If  $\beta \rightarrow \infty$ , show that the answer for part (a) is the same as the one derived in class.  
 (c) For a given  $I$  and  $I_1$ , show that

$$R_1 = \frac{V - V_{BE}}{I_1} \quad \text{and} \quad R_2 = \frac{V_{BE}}{I_1/\alpha - I/\beta}$$

- (d) For  $V_T = 25 \text{ mV}$ ,  $I_S = 7.5 \times 10^{-15} \text{ A}$ ,  $\beta = 99$ , and  $I = 5 \text{ mA}$ , solve for  $R_1$  and  $R_2$  if  $V = 2.4 \text{ V}$  and  $I_1 = 0.1I$ . Answers:  $R_1 = 3.44 \text{ k}\Omega$ ,  $R_2 = 1.49 \text{ k}\Omega$ .  
 (e) Calculate the new values of  $R_1$  and  $R_2$  if the base current in the BJT is neglected. Answers:  $R_1 = 3.44 \text{ k}\Omega$ ,  $R_2 = 1.36 \text{ k}\Omega$ .  
 (f) Repeat part (d) for  $I_1 = 0.9I$ . Answers:  $R_1 = 395 \Omega$ ,  $R_2 = 137 \Omega$ .  
 (g) Calculate the new values of  $R_1$  and  $R_2$  if the base current in the BJT is neglected. Answers:  $R_1 = 395 \Omega$ ,  $R_2 = 138 \Omega$ .

2. The figure shows a circuit for calculating the small-signal resistance of the  $V_{BE}$  multiplier. It is given by  $r = v_t/i_t$ .



- (a) If  $r_0$  is neglected in the small-signal model, use superposition of  $v_t$ ,  $i'_c$ , and  $i_b$  to show that

$$\begin{aligned} i_t &= \frac{v_t}{R_1 + R_2} + i'_c + i_b \frac{R_2}{R_1 + R_2} \\ &= \frac{v_t}{R_1 + R_2} + \alpha i'_e + \frac{i'_e}{1 + \beta} \frac{R_2}{R_1 + R_2} \end{aligned}$$

- (b) With  $r_0$  neglected, replace the BJT with its simplified T model and show that  $i'_e$  is given by

$$i'_e = \frac{v_{tb}}{r'_e} = \frac{v_t R_2}{R_1 + R_2} \frac{1}{r'_e}$$

where  $r'_e$  is calculated with  $R_{tb} = R_1 \parallel R_2$ .

- (c) Combine the above results to show that

$$\begin{aligned} i_t &= \frac{v_t}{R_1 + R_2} \left[ 1 + \frac{R_2}{r'_e} \left( \alpha + \frac{1}{1 + \beta} \frac{R_2}{R_1 + R_2} \right) \right] \\ &= \frac{v_t}{R_1 + R_2} \left[ 1 + \frac{\alpha R_2}{r'_e} \left( 1 + \frac{R_2}{\beta (R_1 + R_2)} \right) \right] \end{aligned}$$

- (d) Add  $r_0$  to the circuit and show that the small-signal resistance reduces to

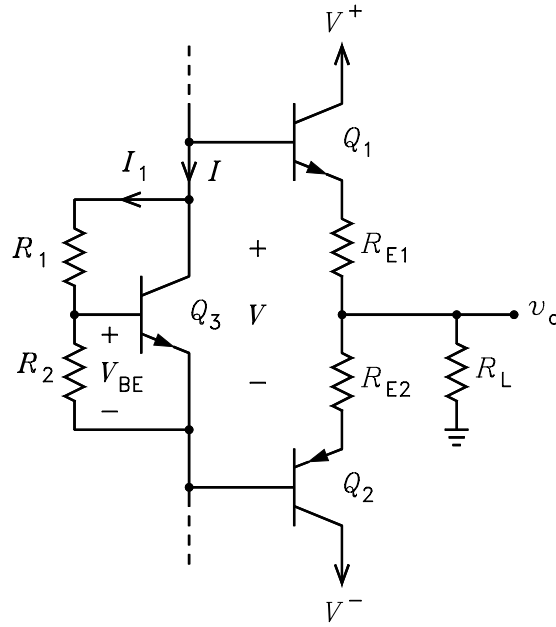
$$r = \frac{v_t}{i_t} = r_0 \parallel r_c \quad \text{where} \quad r_c = \frac{R_1 + R_2}{1 + \frac{\alpha R_2}{r'_e} \left( 1 + \frac{R_2}{\beta (R_1 + R_2)} \right)}$$

- (e) If  $\beta \rightarrow \infty$ , show that the expression for  $r_c$  reduces to

$$r_c = \frac{R_1 + R_2}{1 + R_2/r'_e} = \frac{R_1 + R_2}{1 + g_m R_2}$$

- (f) For the values in Problem 1 part (e) and  $r_x = 40 \Omega$ , calculate  $r_c$ . Answer:  $r_c = 55.1 \Omega$ .  
 (g) For the values in Problem 1 part (f) and  $r_x = 40 \Omega$ , calculate  $r_c$ . Answer:  $r_c = 144 \Omega$ .  
 (h) For the lowest small-signal resistance of the  $V_{BE}$  multiplier, would it be better to bias the BJT at a small fraction of the current  $I$  or at a large fraction? Answer: A large fraction. However, the larger the BJT current, the more sensitive the value of  $R_2$  becomes to the  $\beta$  of the transistor.

3. The figure shows a  $V_{BE}$  multiplier used as a bias source for a complementary CC amplifier. The transistor parameters are the same as those specified in Problem ??.



- For  $v_O = 0$ , solve for  $V_{BE1}$  and  $V_{EB2}$  for  $I_{E1} = I_{E2} = 5 \text{ mA}$ . Answer:  $V_{BE1} = V_{EB2} = 0.68 \text{ V}$ .
- For  $v_O = 0$ , solve for  $R_{E1}$  and  $R_{E2}$  so the voltage across each is equal to 0.1 of the voltage calculated in part (a). Answer:  $R_{E1} = R_{E2} = 13.6 \Omega$ .
- Calculate the required voltage  $V$  across the  $V_{BE}$  multiplier. Answer:  $V = 1.50 \text{ V}$ .
- If  $I = 3 \text{ mA}$  and  $I_1 = 0.1I$ , calculate  $V_{BE3}$ ,  $R_1$ , and  $R_2$  in the  $V_{BE}$  multiplier. Answers:  $V_{BE3} = 0.665 \text{ V}$ ,  $R_1 = 2.77 \text{ k}\Omega$ ,  $R_2 = 2.72 \text{ k}\Omega$ .
- If  $V_A = 70 \text{ V}$  for  $Q_3$ , calculate  $r_0$ ,  $r_c$ , and the small-signal resistance  $r$  of the  $V_{BE}$  multiplier. Answer:  $r_0 = 26.5 \text{ k}\Omega$ ,  $r'_e = 37.3 \Omega$ ,  $r_c = 75.1 \Omega$ ,  $r = 74.9 \Omega$ .
- If  $R_L = 100 \Omega$ , the  $V_{BE}$  multiplier can be approximated by an ac short circuit, and  $Q_1$  and  $Q_2$  have the parameters  $r_0 = 40 \text{ k}\Omega$  and  $r_x = 10 \Omega$ , solve for the voltage gain of the CC stage. Answer:  $A_v = 0.914$ .