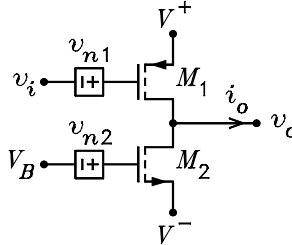


## ECE 6416 Assignment 5

1. A BJT common-emitter amplifier with  $R_E = 0$  is biased at  $I_C = 0.5$  mA. The BJT has a base spreading resistance  $r_x = 50 \Omega$  and a current gain  $\beta = 150$ . A JFET common-source amplifier with  $R_S = 0$  is biased at  $I_D = 0.5$  mA. The JFET has a threshold voltage  $V_{TO} = -2.5$  V and a drain-to-source saturation current  $I_{DSS} = 3$  mA. Flicker noise can be neglected.

- (a) Solve for the signal source resistance  $R_s$  at which the two transistors have the same noise equivalent input voltage  $v_{ni}$ . [2905  $\Omega$ ]
- (b) On the same axes, plot  $v_{ni}$  in  $V/\sqrt{\text{Hz}}$  versus  $R_s$  for a source resistance in the range 100 Hz to 100 kHz. Use log-log scales with a vertical range from  $10^{-9}$  V to  $10^{-7}$  V.
- (c) On the same axes, plot the noise figure  $NF$  versus  $R_s$  for the same range of  $R_s$ . Use dB-log scales with a vertical range from 0 dB to 10 dB. Is the value of  $R_s$  at which the noise figures are equal the same as the value of  $R_s$  at which the equivalent noise input voltages are equal?

2. The figure shows a CMOS amplifier consisting of a p-channel input transistor  $M_1$  and an n-channel load transistor  $M_2$  biased by a fixed gate voltage  $V_B$ .



- (a) Show that the small-signal voltage gain is given by

$$\frac{v_o}{v_i} = -g_{m1} (r_{ds1} || r_{ds2})$$

- (b) Show that the small-signal short-circuit output current is given by

$$i_{o(sc)} = -g_{m1} (v_i + v_{n1}) - g_{m2} v_{n2}$$

- (c) If only flicker noise is modeled, show that the mean-square equivalent noise input voltage is given by

$$v_{ni}^2 = \frac{K_{f1} \Delta f}{2\mu_p L_1 W_1 C_{ox}^2 f} \left[ 1 + \frac{K_{f2}}{K_{f1}} \left( \frac{L_1}{L_2} \right)^2 \right]$$

How should the  $W$  and  $L$  for each device be chosen to minimize the noise? (Choose  $L_2 = L_1 \sqrt{K_{f2}/K_{f1}}$  and make  $L_1$  and  $W_1$  large.)

3. The following MOSFET data are given

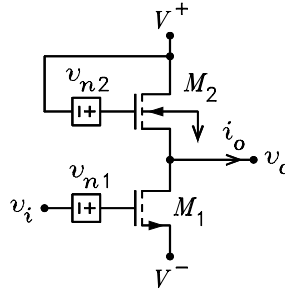
	n-Channel ( $M_2$ )	p-Channel ( $M_1$ )
$\frac{\mu_0 C_{ox}}{2}$	$7 \mu\text{A}/\text{V}^2$	$3 \mu\text{A}/\text{V}^2$
$\frac{K_f}{2\mu_0 C_{ox}^2} \int_{20}^{20k} \frac{df}{f}$	$380 \times 10^3 (\mu\text{V} \times \mu\text{m})^2$	$48 \times 10^3 (\mu\text{V} \times \mu\text{m})^2$

If the value of  $C_{ox}$  is the same for both MOSFETs in the circuit of Problem 2, calculate  $v_{ni}$  for the following values of  $W$  and  $L$ :

	$W_1$	$L_1$	$W_2$	$L_2$
Case 1	$1000 \mu\text{m}$	$5 \mu\text{m}$	$400 \mu\text{m}$	$4 \mu\text{m}$
Case 2	$1000 \mu\text{m}$	$5 \mu\text{m}$	$200 \mu\text{m}$	$8 \mu\text{m}$
Case 3	$500 \mu\text{m}$	$10 \mu\text{m}$	$400 \mu\text{m}$	$4 \mu\text{m}$

( $16.9 \mu\text{V}$ ,  $8.88 \mu\text{V}$ , and  $33.4 \mu\text{V}$ )

4. The figure shows an n-channel NMOS enhancement-mode common-source amplifier with an active n-channel NMOS enhancement-mode load. The two transistors are biased at the same drain current  $I_D$  and have the same value for  $C_{ox}$ .



(a) Show that the small-signal short-circuit output current is given by

$$i_{o(sc)} = -g_{m1}(v_i + v_{n1}) + g_{m2}v_{n2}$$

(b) Show that the small-signal output resistance is given by

$$r_{out} = r_{ds1} \parallel r_{ds2} \parallel \left( \frac{1}{g_{m2}(1 + \chi_2)} \right)$$

(c) Show that the open-circuit output voltage is given by

$$v_{o(oc)} = (-g_{m1}(v_i + v_{n1}) + g_{m2}v_{n2}) \times r_{ds1} \parallel r_{ds2} \parallel \left( \frac{1}{g_{m2}(1 + \chi_2)} \right)$$

- (d) If only flicker noise is modeled, show that the mean-square equivalent noise input voltage is given by

$$v_{ni}^2 = \frac{K_{f1}\Delta f}{2\mu_n C_{ox}^2 L_1 W_1 f} \left[ 1 + \left( \frac{L_1}{L_2} \right)^2 \right]$$

It is obvious that  $W_1$  should be large to minimize the noise. What should  $L_1$  be to minimize the noise? ( $L_1 = L_2$ )

- (e) If only thermal noise is modeled, show that the mean-square equivalent noise input voltage is given by

$$v_{ni}^2 = \frac{4kT\Delta f}{3\sqrt{K_1 I_D}} \left[ 1 + \sqrt{\frac{L_1 W_2}{L_2 W_1}} \right]$$

How should the  $W$  and  $L$  for each device be chosen to minimize the noise? ( $L_2$  and  $W_1$  should be large and  $L_1$  and  $W_2$  should be small)

5. Repeat problem 3 for part (d) of problem 4. ( $14.0 \mu\text{V}$ ,  $10.3 \mu\text{V}$ , and  $23.5 \mu\text{V}$ )
6. A common-source MOSFET amplifier is driven by a source with an output resistance  $R_s = 50 \Omega$ . The MOSFET has the parameters  $g_m = 2 \text{ mS}$  and  $c_{gs} = 1.5 \text{ pF}$ . The frequency is  $f = 900 \text{ MHz}$ . It can be assumed that  $c_{gd}$  has been “tuned out” by the addition of a suitable matching network in parallel with the input.
- (a) Calculate the value of an inductor  $L_s$  in series with the source which will give a resistance looking into  $c_{gs}$  from the gate of  $50 \Omega$ . [ $0.0375 \mu\text{H}$ ]
- (b) Calculate the noise figure  $NF$  of the circuit. [ $8.10 \text{ dB}$ ]
- (c) If the value of  $L_s$  is chosen to make the gate input impedance real, i.e. to cancel  $c_{gs}$ , and  $g_m$  is varied to obtain an impedance match with the source, calculate the new values of  $L_s$ ,  $g_m$ , and  $NF$ . [ $0.0209 \mu\text{H}$ ,  $3.60 \text{ mS}$ ,  $2.22 \text{ dB}$ ]